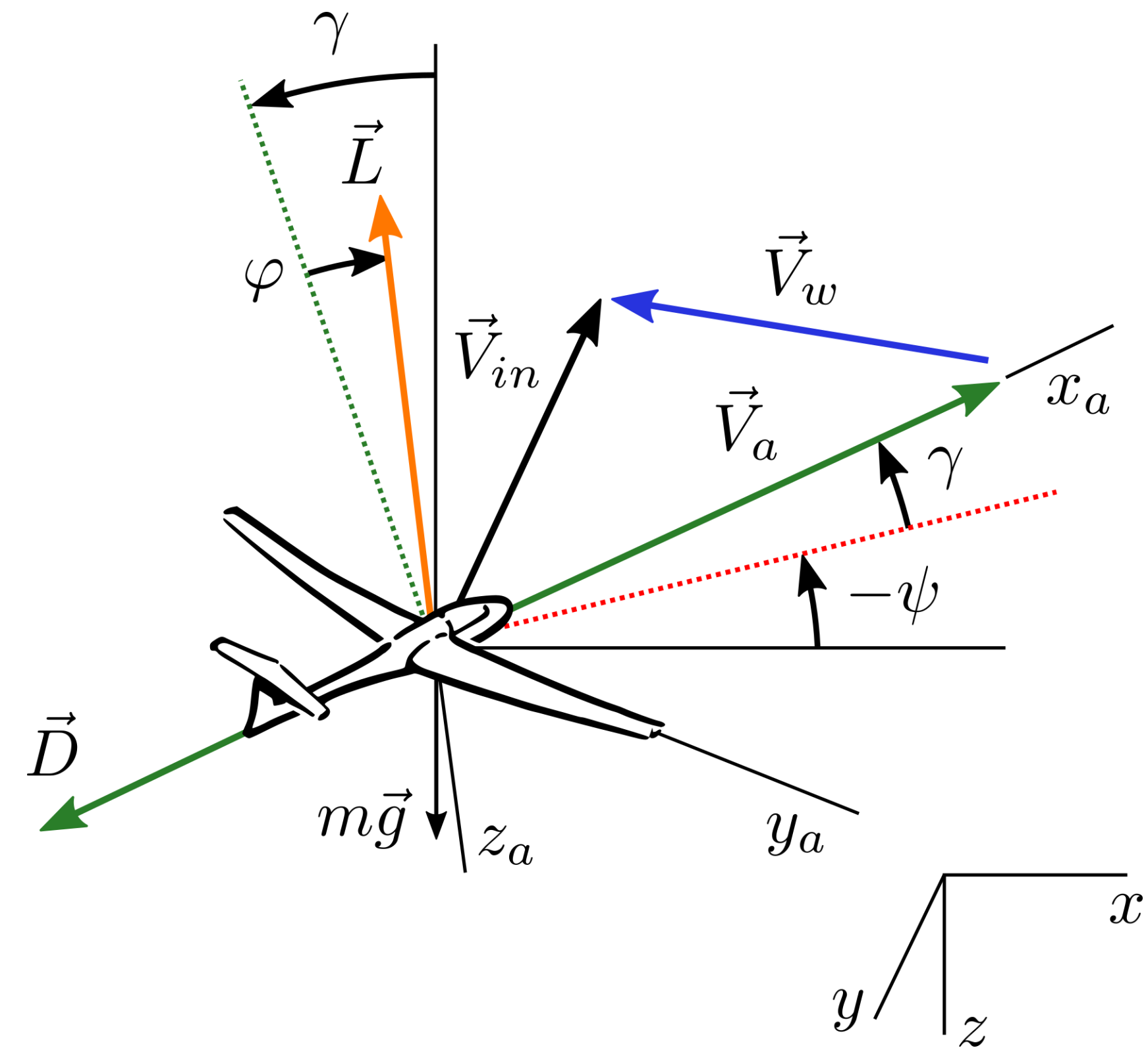


Atmospheric Flight Mechanics on Other Planets



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Equations of Motion and Optimal Trajectories



- Three degree of freedom sailplane model with parameters ($C_{Lmax} = 0.8, C_{D0}, C_L/C_{D|max}$) and scaling $V = \sqrt{\frac{mg}{0.5\rho S}}, Z = \frac{m}{0.5\rho S}, T = \sqrt{\frac{m}{0.5\rho Sg}}$, allows for the governing equations:

$$\vec{V}'_{in} = \vec{V}'_a + \vec{V}'_w = \begin{bmatrix} \dot{x}' \\ \dot{y}' \\ \dot{z}' \end{bmatrix} = V'_a \begin{bmatrix} \cos(\psi)\cos(\gamma) \\ \cos(\gamma)\sin(\psi) \\ -\sin(\gamma) \end{bmatrix} + \begin{bmatrix} V'_{wx} \\ V'_{wy} \\ V'_{wz} \end{bmatrix}$$

$$\begin{aligned} \dot{V}'_a &= -D^* - \sin(\gamma) + \dot{V}'_{wz} \sin(\gamma) - \dot{V}'_{wy} \sin(\psi) \cos(\gamma) - \dot{V}'_{wx} \cos(\gamma) \cos(\psi) \\ V'_a \dot{\gamma}' &= L^* \cos(\varphi) - \cos(\gamma) + \dot{V}'_{wy} \sin(\gamma) + \dot{V}'_{wx} \sin(\gamma) \cos(\psi) + \dot{V}'_{wz} \cos(\gamma) \\ V'_a \cos(\gamma) \dot{\psi}' &= L^* \sin(\varphi) + \dot{V}'_{wx} \sin(\psi) - \dot{V}'_{wy} \cos(\psi) \end{aligned}$$

Optimal trajectory is sought with objective function

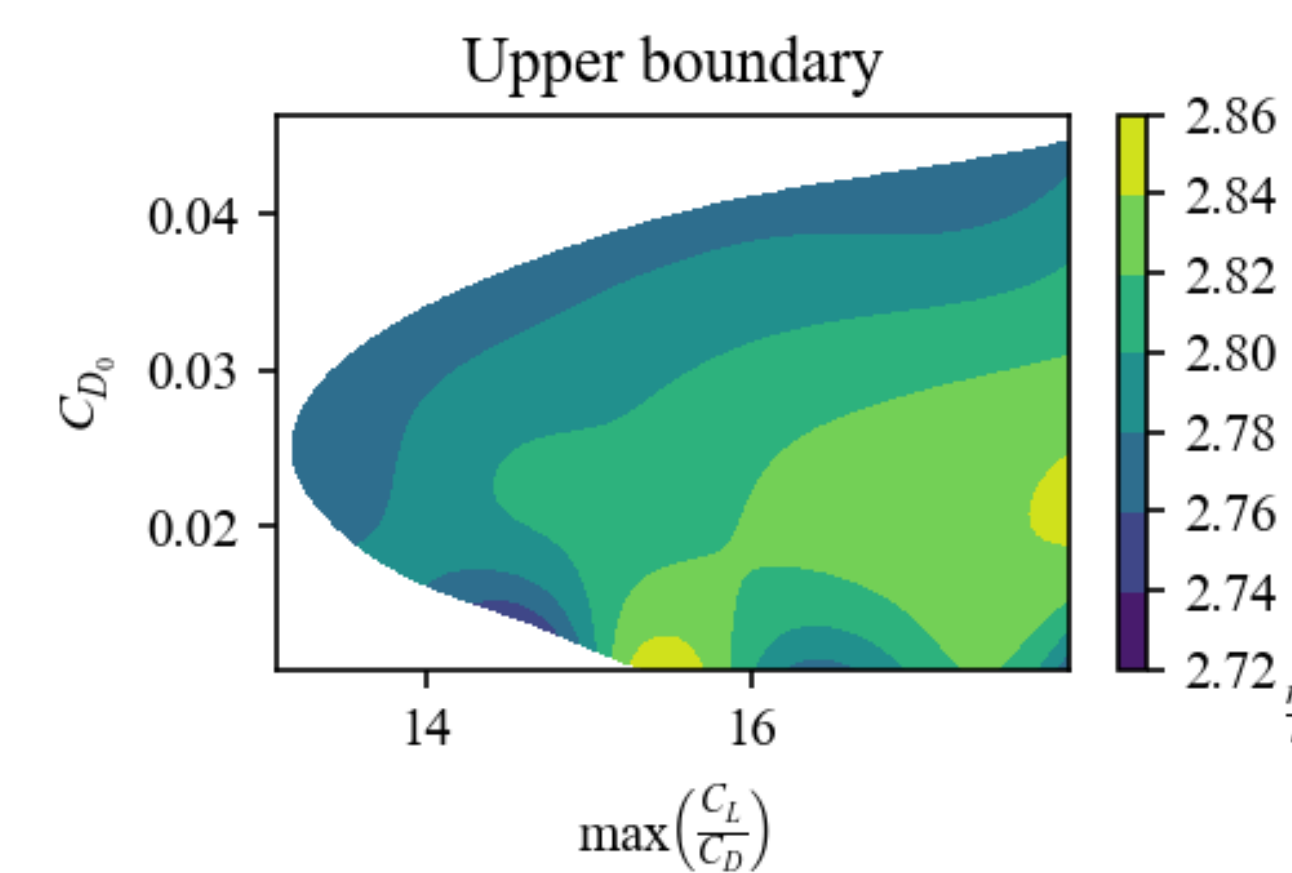
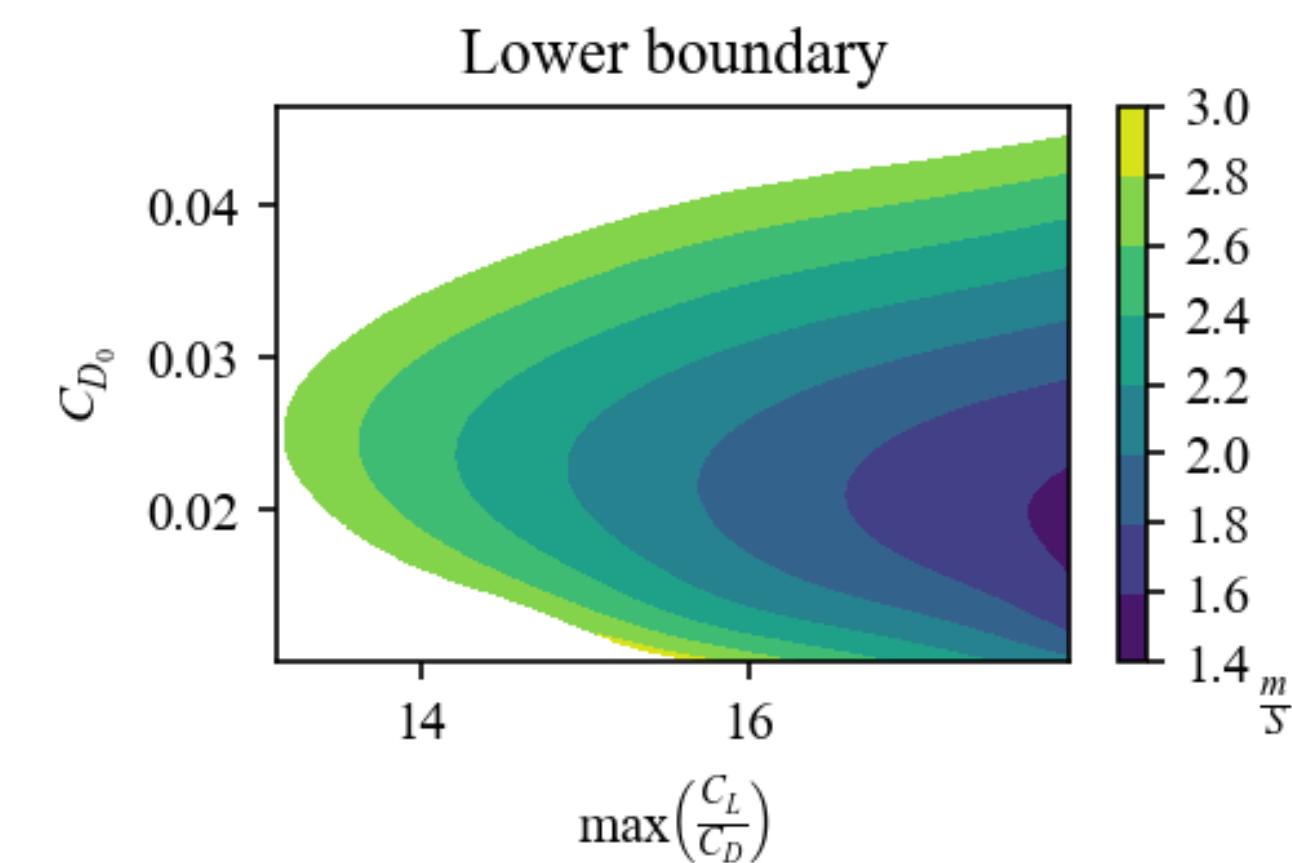
$$\max_{C_L, \varphi} \left\{ \frac{d}{dt} (0.5V'_a{}^2) : \forall t' \right\}$$

subjected to constraints

$$z' < 0; \quad V'_{stall} < V'_a; \quad z'_{t=0} = z'_{t_f}; \quad \psi'_{t=0} = \psi'_{t_f}$$

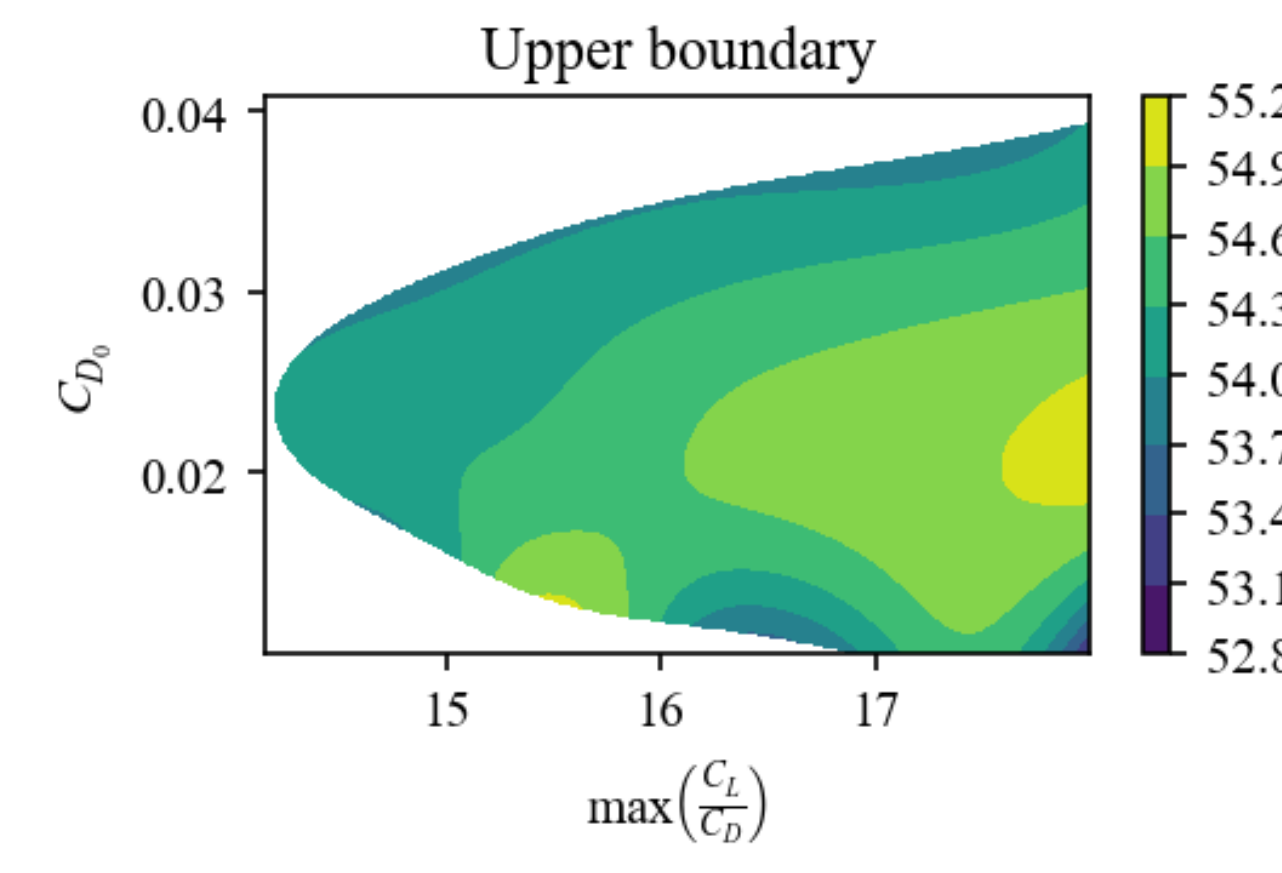
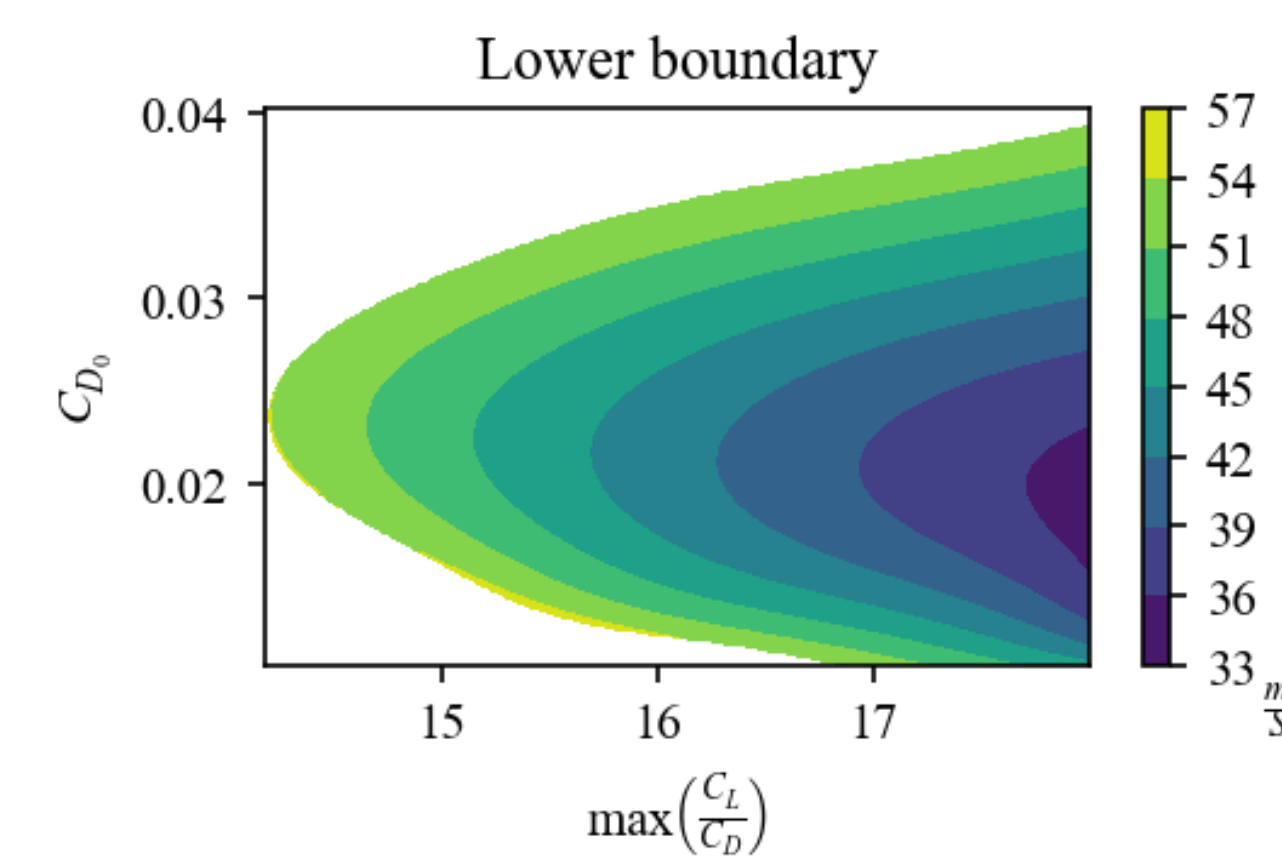
Mars at ground level: $\rho = 0.0137 \text{ kg/m}^3$
 $g = 3.711 \text{ m/s}^2 \quad \partial V_{wx}/\partial z \approx 40 \text{ m/s/km}$

m/S contours for energy positive dynamic soaring
 $h_{shear} = 600 \text{ m}$



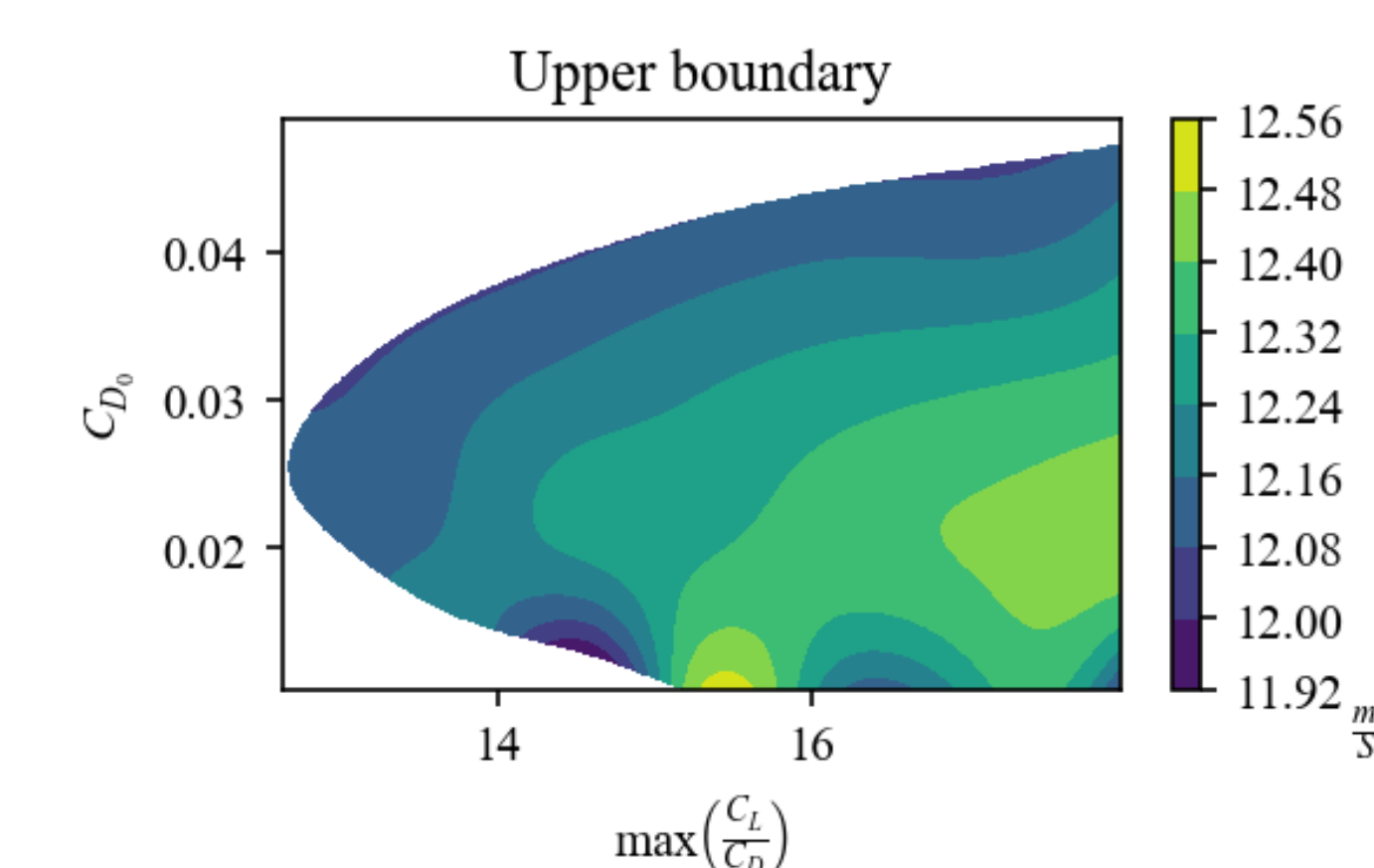
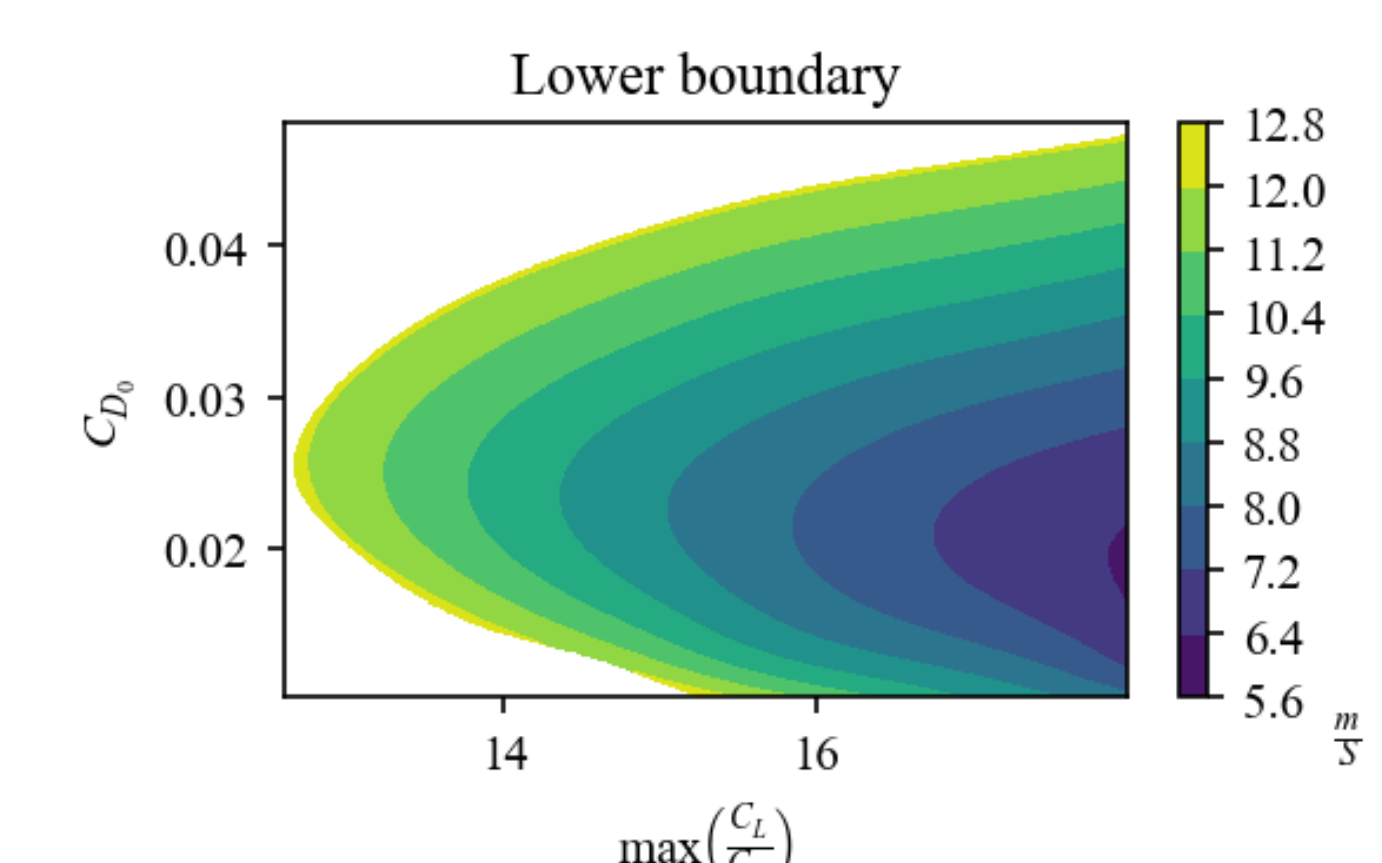
Titan at ground level: $\rho = 5.3 \text{ kg/m}^3$
 $g = 1.35 \text{ m/s}^2$

m/S contours for energy positive dynamic soaring
 $h_{shear} = 30 \text{ m}, \partial V_{wx}/\partial z = 100 \text{ m/s/km}$



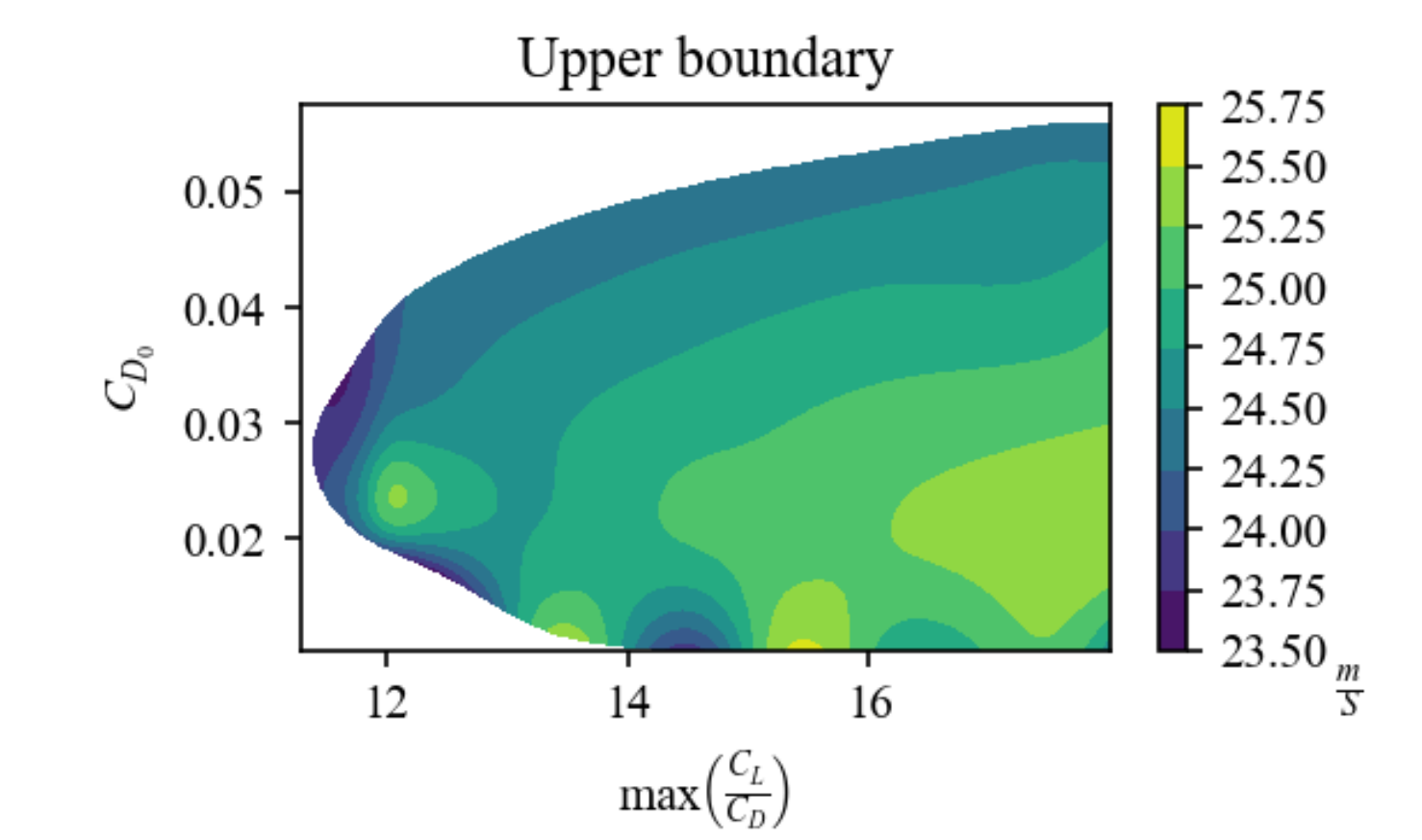
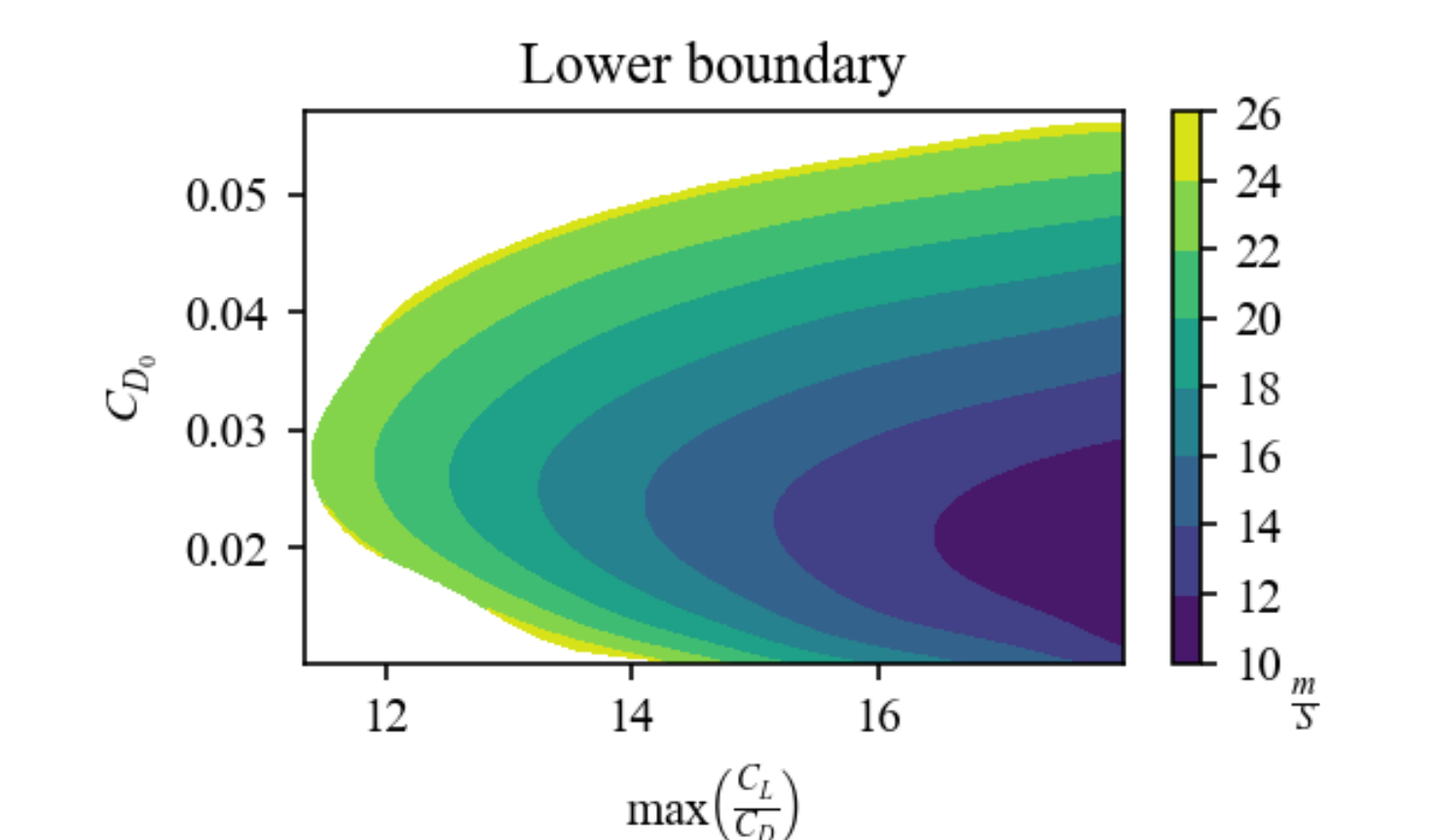
Titan in shear layer (80km): $\rho = 0.06 \text{ kg/m}^3$
 $g = 1.35 \text{ m/s}^2$

m/S contours for energy positive dynamic soaring
 $h_{shear} = 600 \text{ m}, \partial V_{wx}/\partial z = 25 \text{ m/s/km}$



Venus in shear layer (50km): $\rho = 1.46 \text{ kg/m}^3$
 $g = 8.87 \text{ m/s}^2$

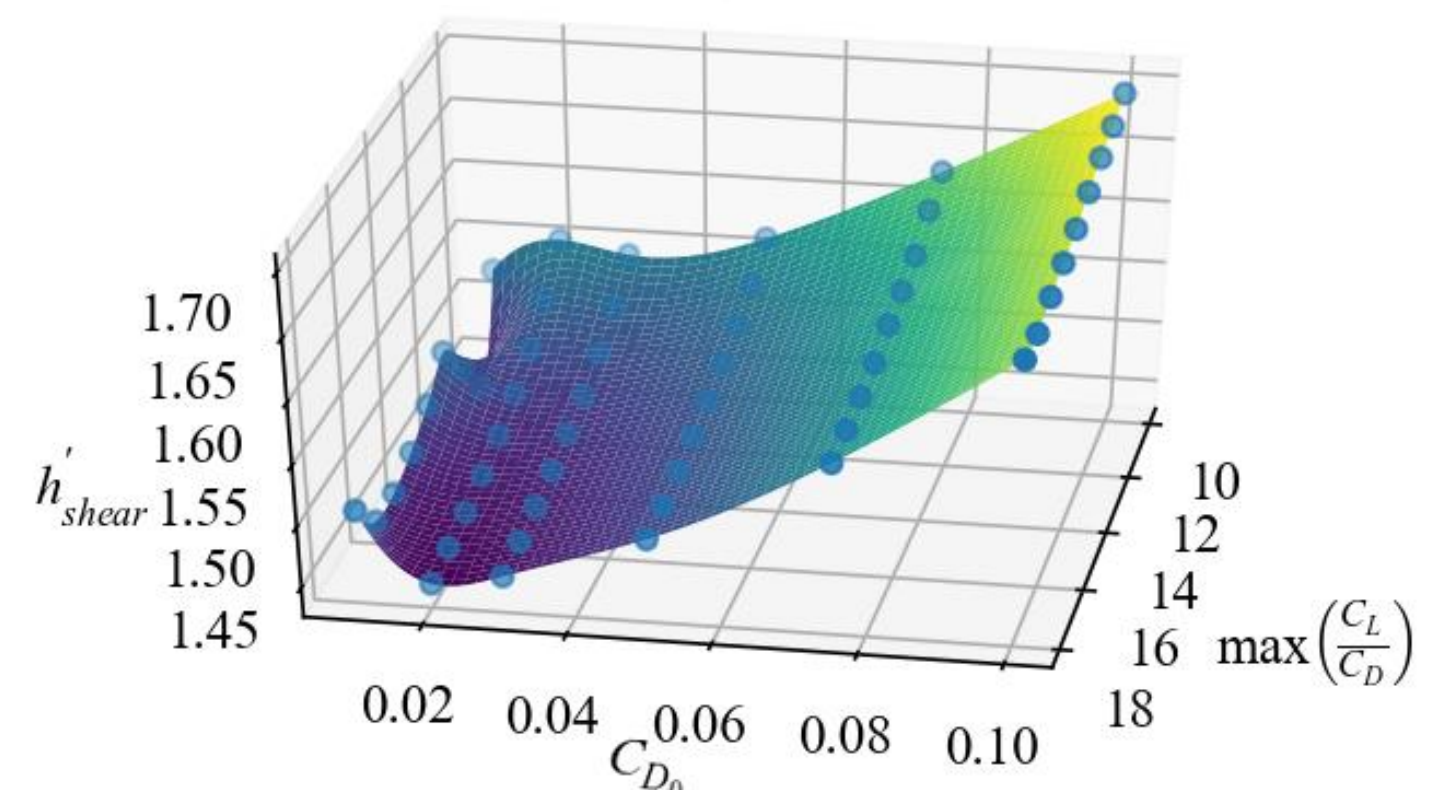
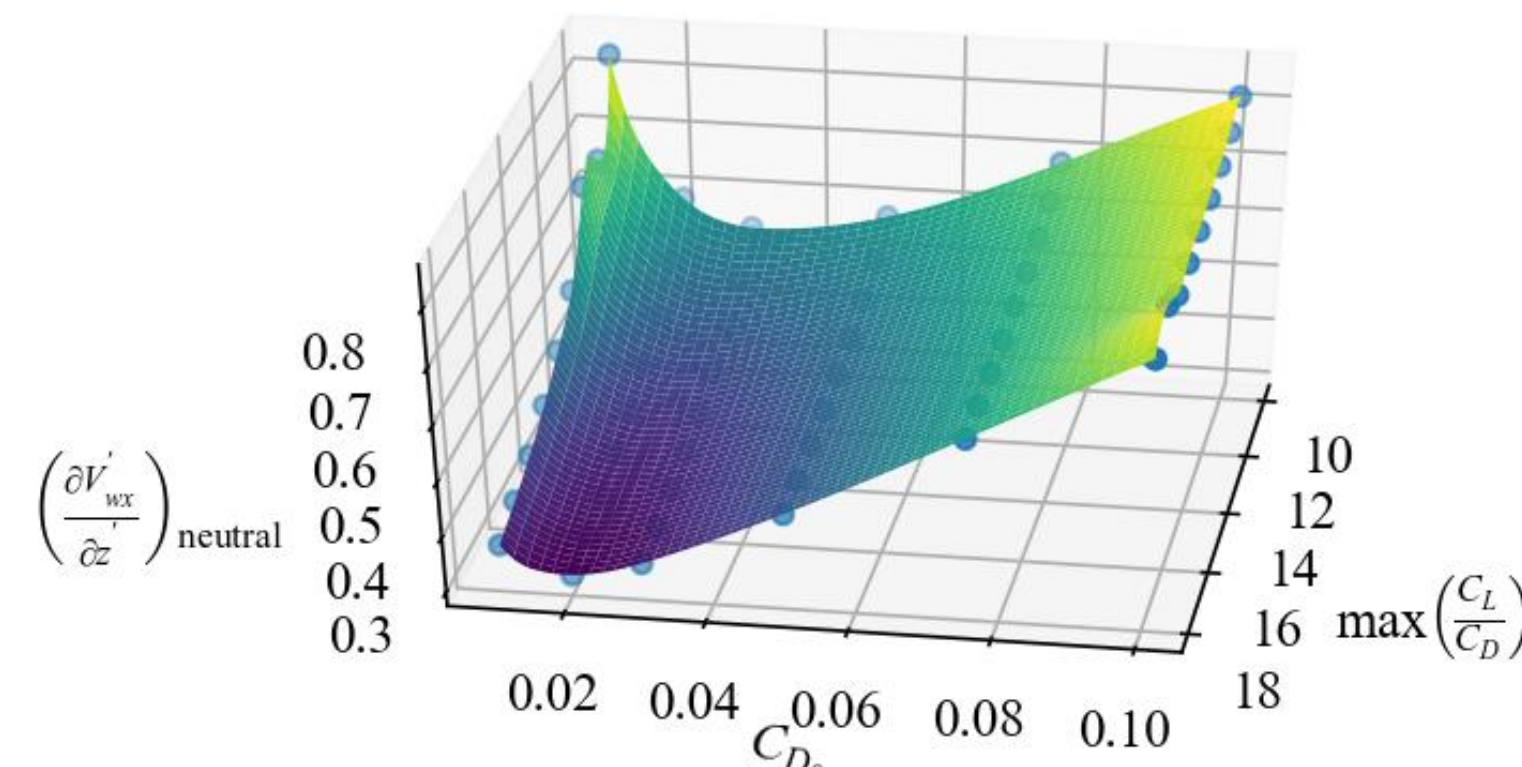
m/S contours for energy positive dynamic soaring
 $h_{shear} = 50 \text{ m}, \partial V_{wx}/\partial z = 250 \text{ m/s/km}$



Dynamic Soaring in Atmosphere of Mars, Titan, Venus

Comparative study approach

- Assuming linear and unidirectional wind function $V'_{wx} = z' \frac{\partial V'_{wx}}{\partial z'} + V'_{wx0}$
- Solving optimal trajectory problem for $C_{Lmax} = 0.8; C_{D0} = [0.01, 0.02, \dots, 0.1]; C_L/C_{D|max} = [10, 11, \dots, 20]$
- To find $\frac{\partial V'_{wx}}{\partial z'} (C_{D0}, C_L/C_{D|max})$ for the energy neutral cycle, such that total energy at initial and final time instants stay the same

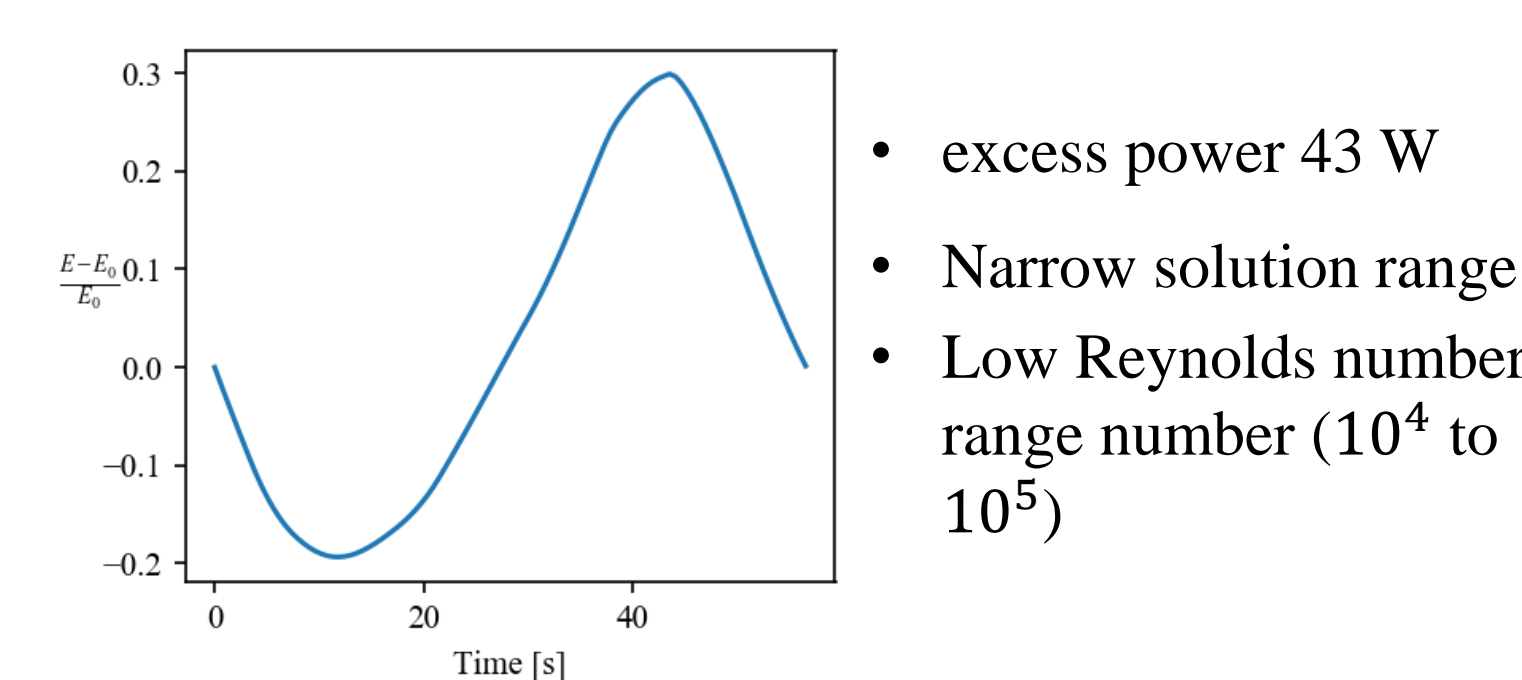
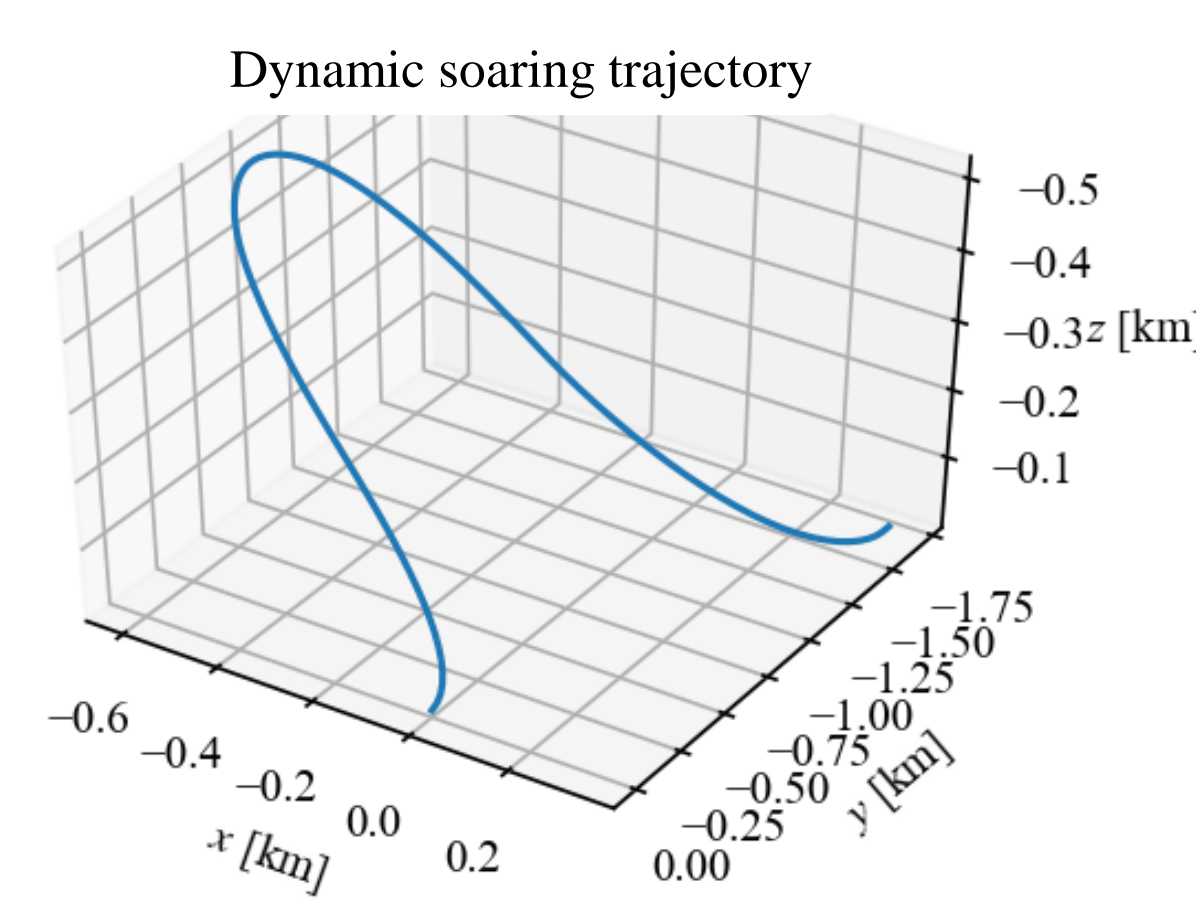


Based on the results for $\left(\frac{\partial V'_{wx}}{\partial z'}\right)_{neutral}$, and corresponding $h'_{neutral}$, sufficient conditions on the neutral energy cycle are found

$$\frac{\left(\frac{\partial V'_{wx}}{\partial z'}\right)_{neutral}^2}{\left(\frac{\partial V'_{wx}}{\partial z'}\right)_{shear}^2} \leq \frac{0.5\rho g}{S} \leq \frac{m}{S} \leq \frac{h'_{shear} 0.5\rho}{h'_{neutral}}$$

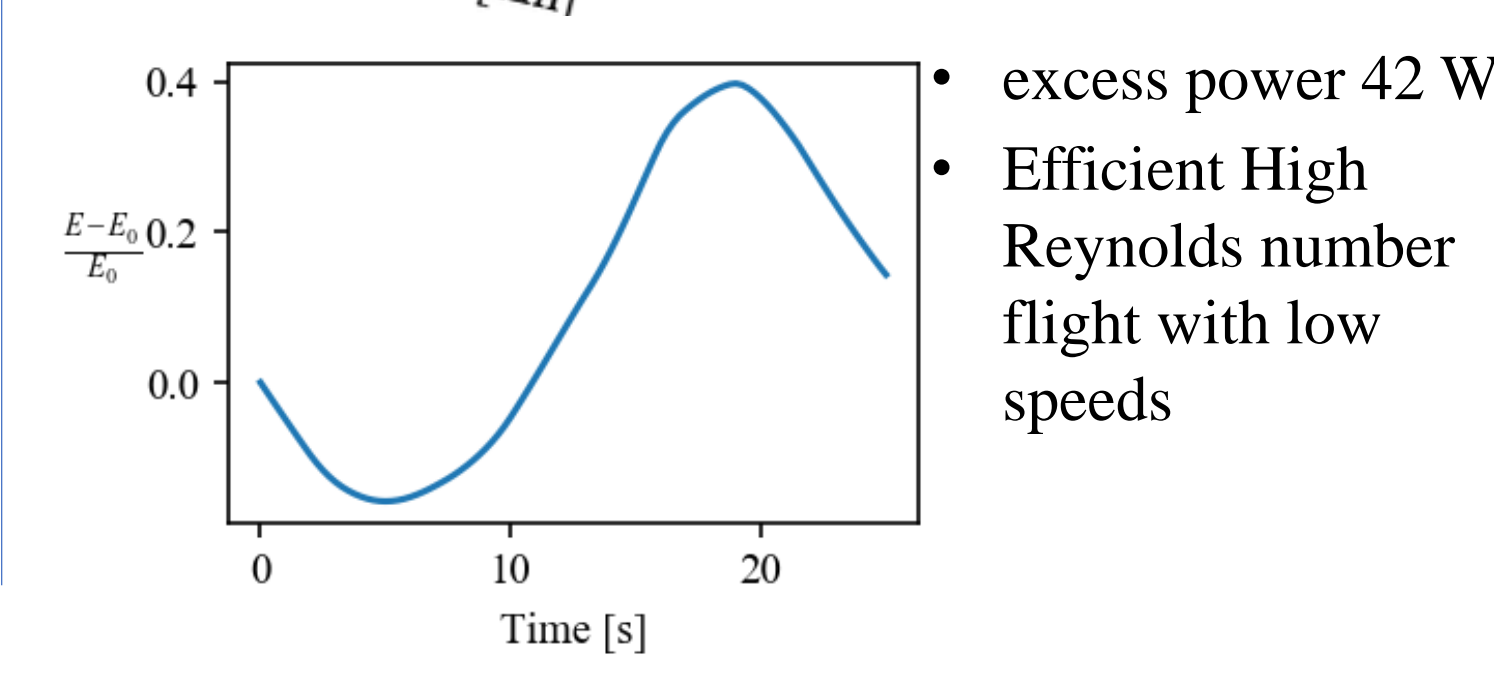
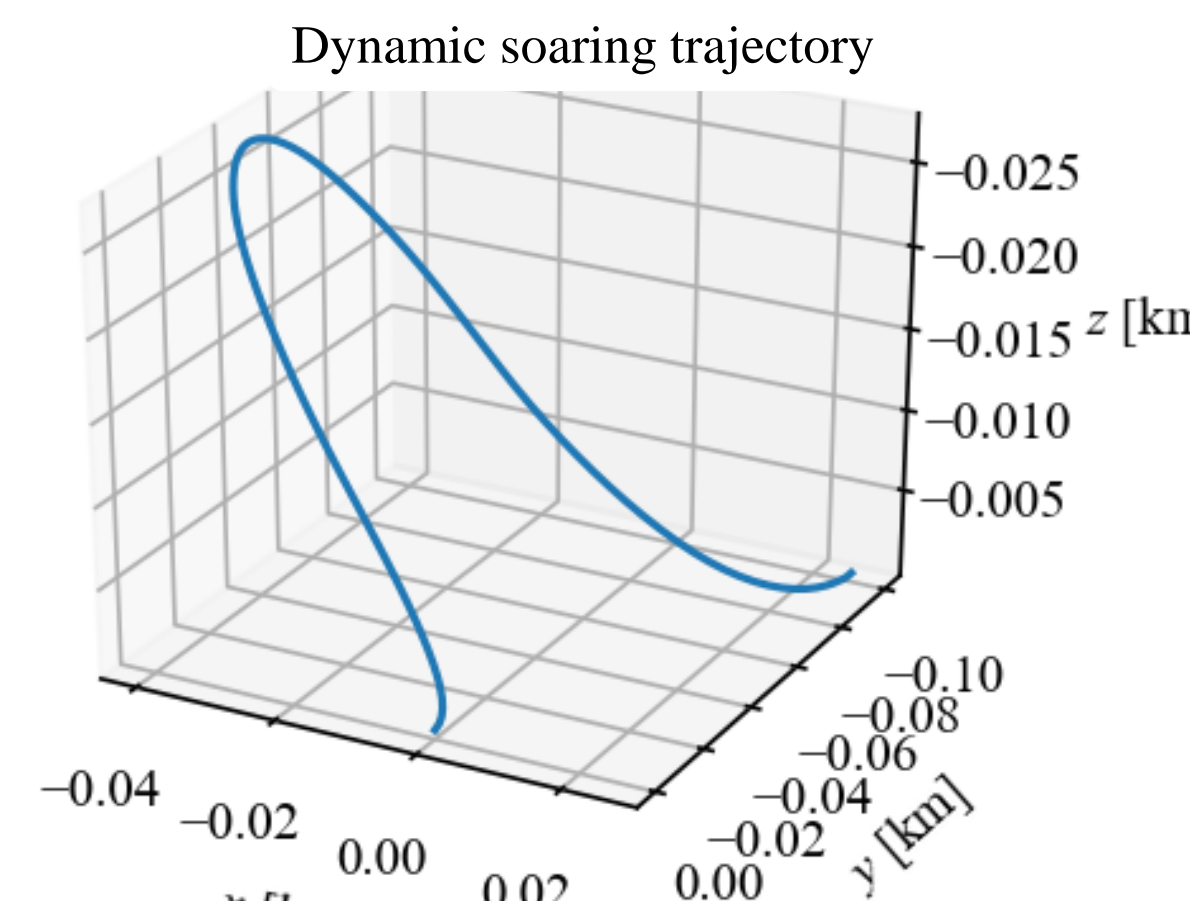
Sailplane Designs

$S = 4.46 \text{ m}^2$ $m = 5 \text{ kg}$ $C_L/C_{D|max} = 14.4$
 $C_{D0} = 0.027$ Wingspan = 5 m $\partial V_{wx}/\partial z = 40 \text{ m/s/km}$



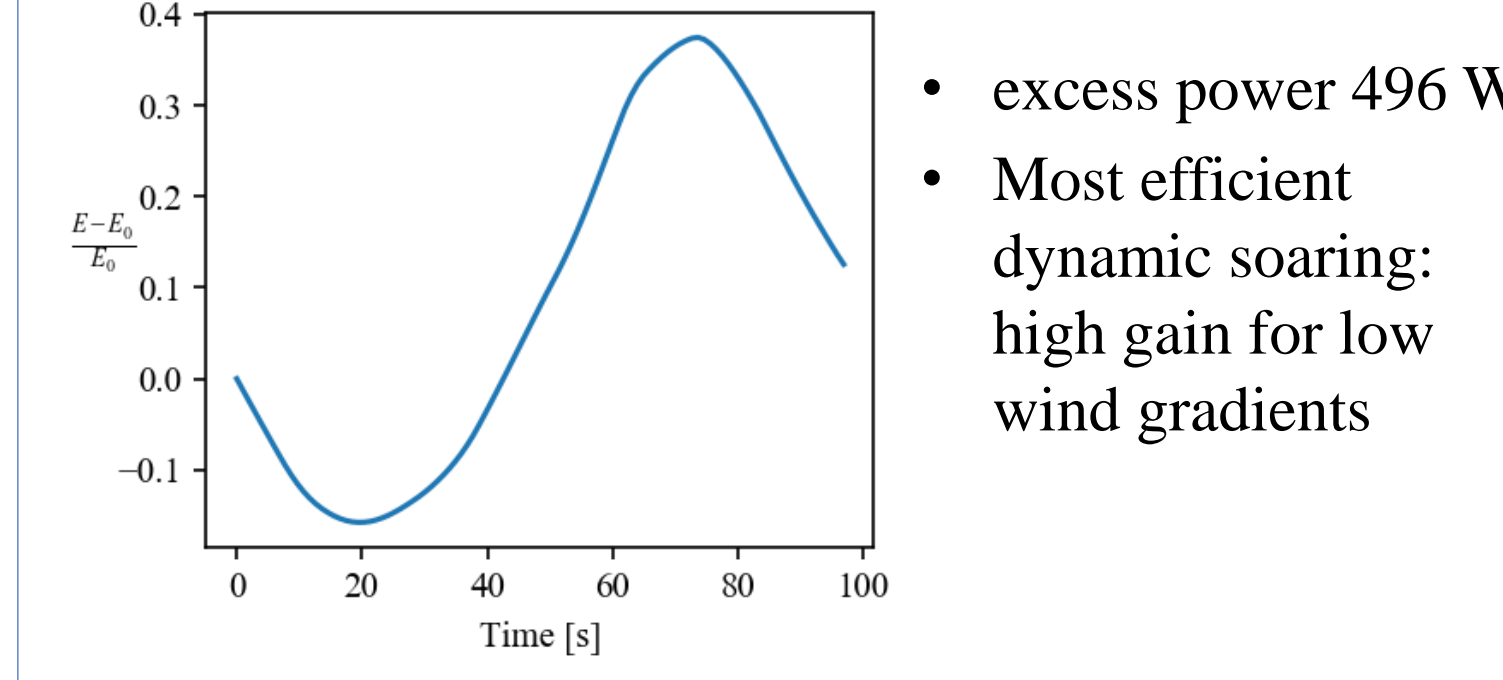
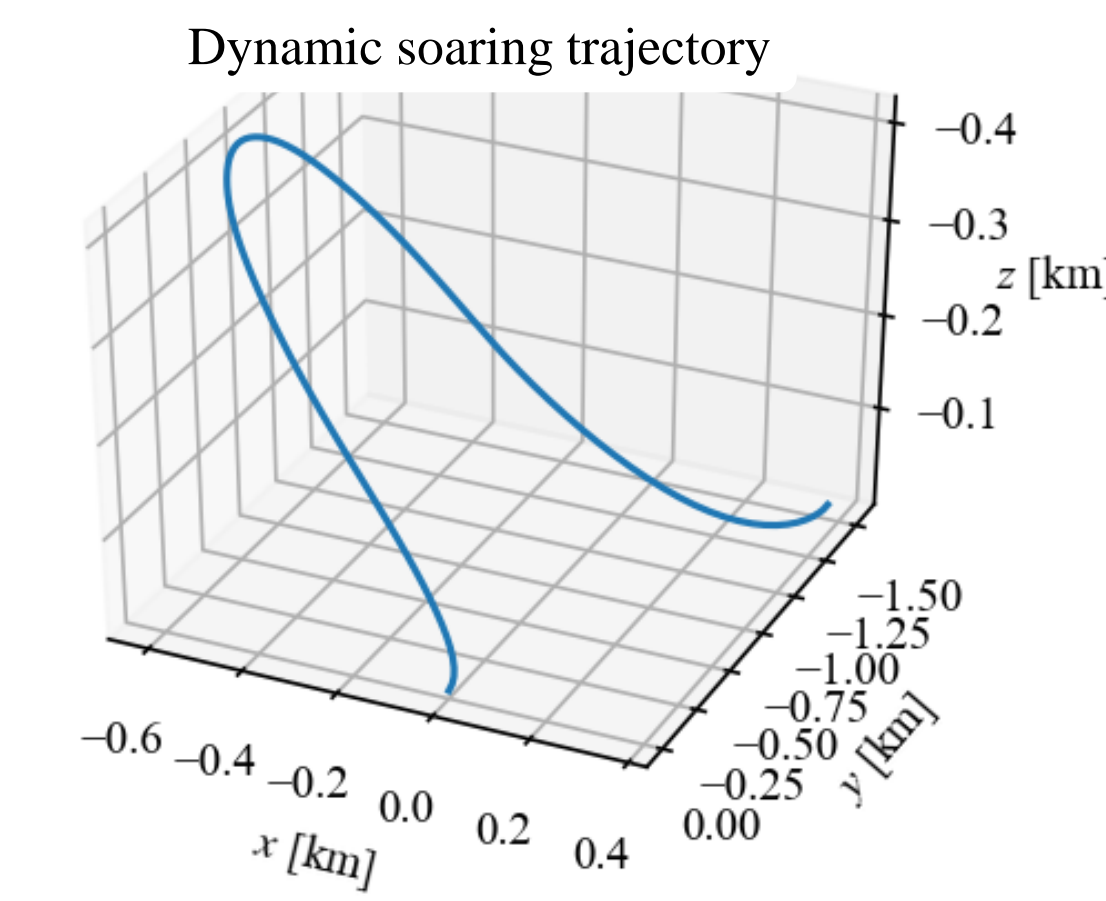
- excess power 43 W
- Narrow solution range
- Low Reynolds number range number (10^4 to 10^5)

$S = 0.125 \text{ m}^2$; $m = 5 \text{ kg}$; $C_L/C_{D|max} = 20$
 $C_{D0} = 0.015$; Wingspan = 1.0 m; $\partial V_{wx}/\partial z = 100 \text{ m/s/km}$



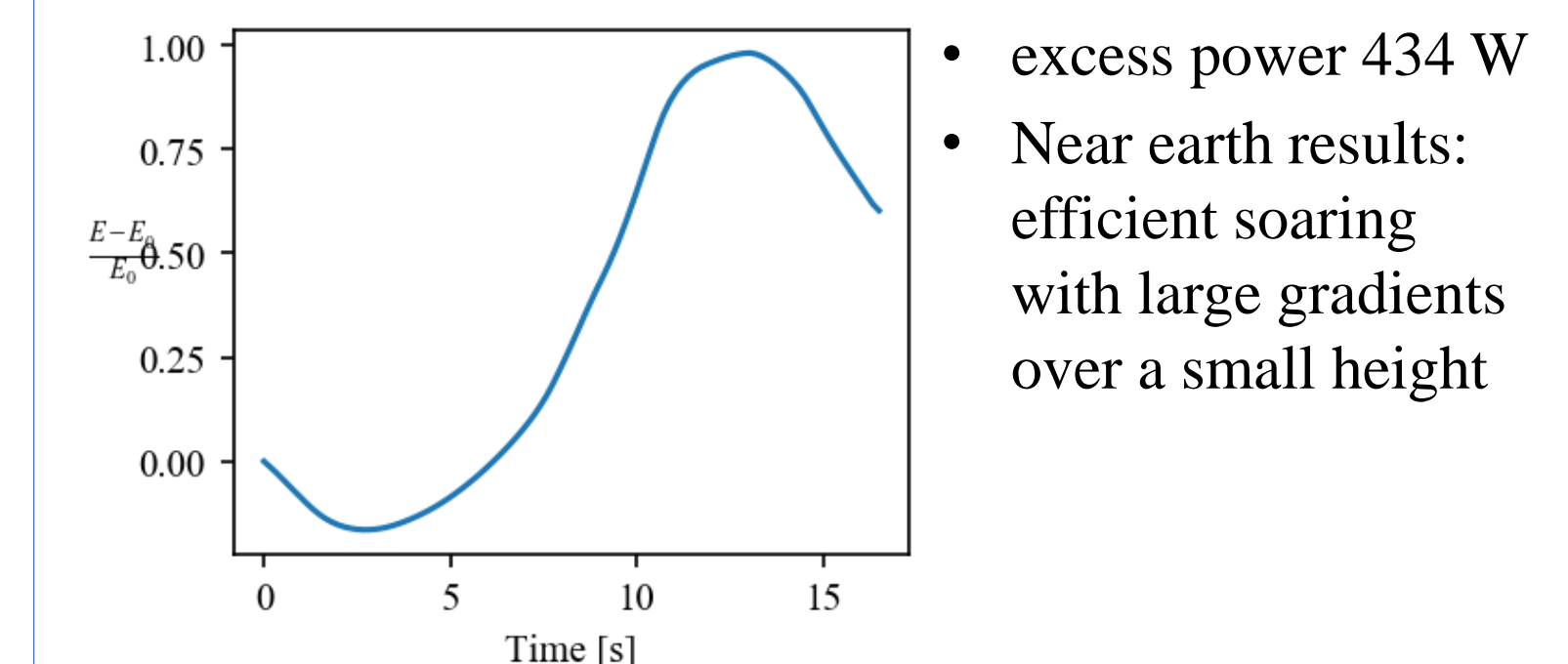
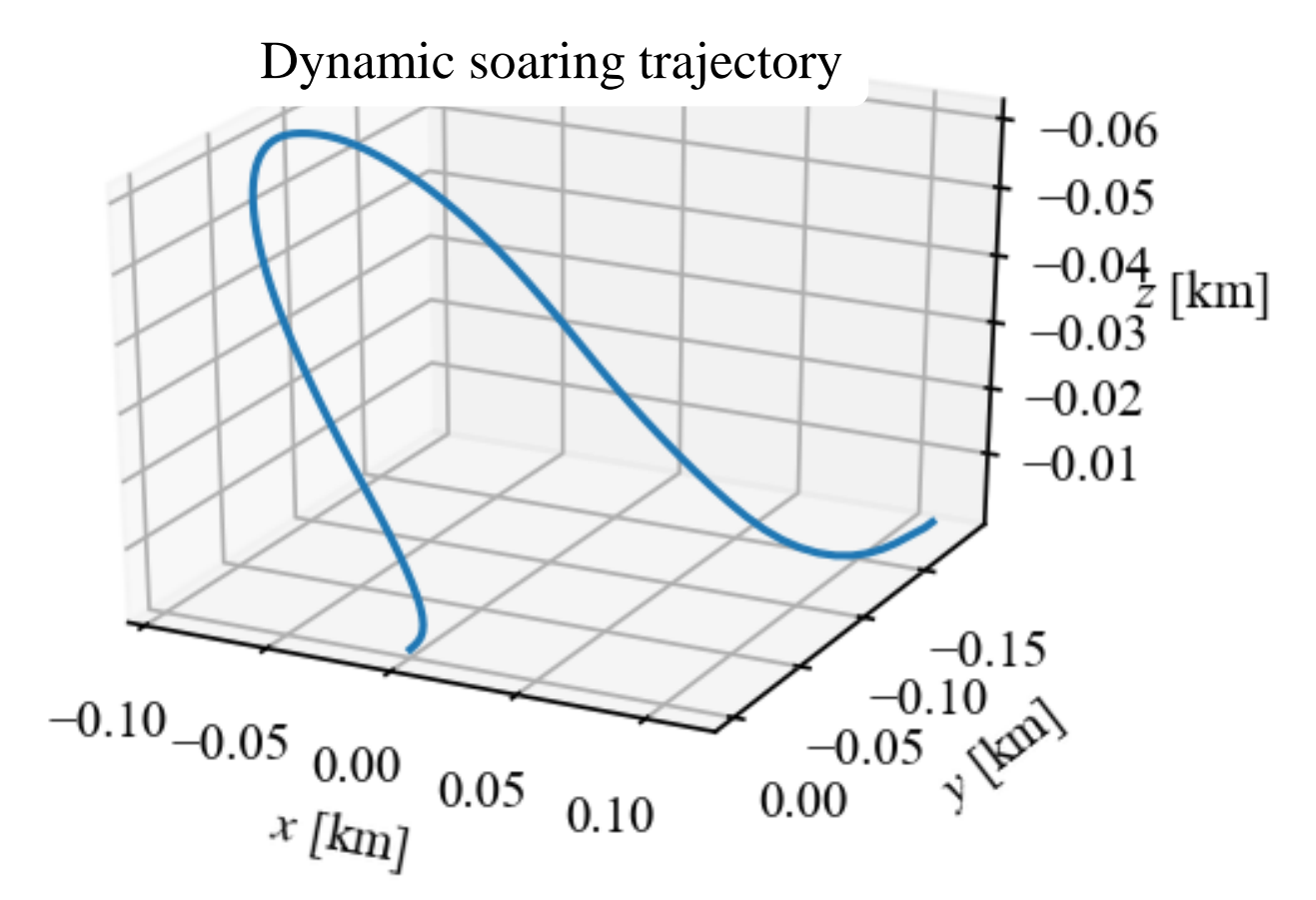
- excess power 42 W
- Efficient High Reynolds number flight with low speeds

$S = 0.5 \text{ m}^2$; $m = 3.5 \text{ kg}$; $C_L/C_{D|max} = 19.25$
 $C_{D0} = 0.015$; Wingspan = 1.7 m; $\partial V_{wx}/\partial z = 25 \text{ m/s/km}$



- excess power 496 W
- Most efficient dynamic soaring: high gain for low wind gradients

$S = 0.4 \text{ m}^2$; $m = 5 \text{ kg}$; $C_L/C_{D|max} = 20$
 $C_{D0} = 0.015$; Wingspan = 1.5 m; $\partial V_{wx}/\partial z = 250 \text{ m/s/km}$



- excess power 434 W
- Near earth results: efficient soaring with large gradients over a small height

Conclusions

- The algorithm for comparative dynamic soaring cycles studies has been developed based on three degrees of freedom and linear unidirectional wind models. It allows expression of energy positive trajectories in various atmospheres.
- Sufficient conditions for the energy positive dynamic soaring are established providing wind shear gradients and altitude range. Higher density atmosphere requires greater wind gradients over smaller heights for sailplane designs with wing loading ranging from 1 to 60.
- Dynamic soaring is feasible on Mars with a narrow wing loading range. It requires a larger sailplane than for Titan or Venus, where it is easier to achieve within the given conditions in high altitude shear layers. Future studies are needed involving higher fidelity wind data.

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